Soot formation during polyurethane (PU) plastic pyrolysis: the effects of temperature and volatile residence time

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ABSTRACT

Soot is an undesired co-product during thermal-chemical disposal (incineration, pyrolysis, etc.) of plastic wastes at high temperatures, while also regarded as a valuable nanoscale carbon-based material if with proper production and post-treatment methods. In this paper, the pyrolysis of polyurethane (PU) plastics, a major composition of plastic waste, was conducted in a fixed-bed reactor to investigate the soot formation mechanism in depth. The effects of pyrolysis temperature (1000-1300 °C) and volatile residence time (0.2-2 s) on the yield, micro-morphology, composition and reactivity of soot were studied. Results show that the initialization and growth of soot particles during PU pyrolysis requires a certain high temperature and long volatile residence time. With a volatile residence time of 2 s, the soot yield is 11.0 wt.% at 1000 °C and increases to 24.5 wt.% with the pyrolysis temperature increasing to 1300 °C; while when the volatile residence time decreases to 0.2 s, the soot cannot be observed until 1200 °C. When the pyrolysis temperature increases 1000 °C to 1100 °C, the X-ray diffraction (XRD) patterns indicates an enhanced graphitization thereby a lower reactivity of soot oxidation, which is approved by onion-like layered structures initially observed by the high-resolution transmission electron microscope (HR-TEM) at 1100 °C and 2 s. When the pyrolysis temperature increases from 1100 °C to 1200-1300 °C, NaCl is observed in soot particles, which catalysis promotes the reactivity of soot oxidation. Gas chromatography and mass spectrometer (GC-MS) was used to measure the gas and tar compositions, especially the polycyclic aromatic hydrocarbons (PAHs), are proved essential for the formation of soot precursor. A large number of PAHs with ring number ≥ 4 start to form at 1100-1200 °C. Based on the soot characterization and gas-tar compositions, a pathway from light fragments and mono-ring aromatics to heavier aromatic compounds is proposed aiming to explain the chemical evolution of soot precursor particles.

Keywords: Polyurethane; pyrolysis; soot; volatile residence time; high temperature.

1. Introduction

Providing a fundamental contribution to various modern daily activities, plastics have become essential materials in agriculture, automobile industry, electricity and electronics, construction industry and so on [1]. Among them is polyurethane (PU) plastic, which is an important kind of copolymer containing blocks of polyesters or polyethers of low molecular weight cobalently bonded by a urethane group (–NHCO–O–), widely used in the manufacture of car paints, flexible foams for bedding, rigid foams for insulation, adhesives and other commercial goods [2], and its production has reached 16 million tons per year since 2015. The production of polyurethane plastics of large quantity among which only a small amount is recycled, the majority being not biodegradable, however, leads to an increasing generation of waste. A prevalent way to dispose of wasted PU plastic is landfilling, which induces severe air, water, and soil pollutions [3]. While incineration is normally connected to waste-to-energy management and once considered economical and of high energy recovery rate [4], it is now questioned due to its emission of smoke (particulate matter), particulate-bound heavy metals and volatile organic compounds [5]. Therefore, the adoption of more efficient and environmental-friendly methods is highly urged.

Upgrading of plastic waste through pyrolysis is regarded as one of the most environmental and sustainable treatment methods, since neither will the unbiodegradable deposition be remained nor will the organic compounds in the feedstock be wasted. Being in an inert atmosphere (free from oxygen), pyrolysis succeeds in realizing high efficiency of energy conversion and low emission properties, surpassing the combustion/incineration or gasification methods due to the high energy recover rate, avoided forming pollutant and reduced carbon footprints [6]. In pyrolysis, the thermal cracking processes of polymeric materials under high temperatures lead to the breakdown of macromolecular structures and the formation of a wide range of hydrocarbons. When under modest temperature conditions, three fractions composing of a gas fraction, a liquid fraction, i.e. tar, mainly consisting of paraffins, olefins, naphthenes and aromatics, and a solid residue, i.e. char, are divided from the pyrolytic products. Plenty of studies have reported the investigations on these valuable products including upgraded bio-oil as high quality liquid fuels [7, 8], syngas with high heating value [9, 10] and char for agricultural and catalytic use [11]. To sum up, the distribution of products and their properties from plastic pyrolysis are highly dominated by a series of factors including temperature, pressure, residence time, reactor time and feedstock, etc. [12].

While gas/tar/char products of plastic pyrolysis being extensively studied, another product, soot, which occurs only when pyrolysis temperature is elevated highly enough [13], is raising wide attention. Soot is a highly carbonized, solid-phase compound with a particle size scale of nanometer, in which the carbon mole fraction is over 0.85 [14]. Due to its small particle size, high diffusivity and strong sorption capacity of heavy metals and toxic larger polycyclic aromatic

hydrocarbons (PAHs), soot has become a severe threaten to atmospheric environment and human health, thus a major concern in pollutant emission control. Sufficient studies have confirmed the close relationship between soot formation and pyrolysis volatiles which is mainly dominated by two mechanisms, that is, the hydrogen abstraction/carbon addition (HACA) mechanism [15] and a "ring-ring condensation" interaction [16]. Further surface growth, coalescence and agglomeration lead to the final appearance of soot particles whose diameters are about 20-200 nm, in terms of chains, clusters, dendrites, rings, spheroids, flakes and other types [17]. Physical and chemical characteristics of soot particles, such as the inception particle size, structure of the aggregates and soot reactivity, highly depend on the types of fuels whose varied chemical compositions lead to totally different reaction pathway, and reaction conditions which determine the circumstances the soot particles originate. For instance, a wide variation of temperature allows a shift of soot particle size distribution to be observed [18], while under higher pressure the particles were compressed to form small smooth pellets [17]. Soot yields and morphologies also showed huge differences when different feedstock was used [13]. In summary, though large quantities of previous researches exist, the precise mechanisms of how soot properties are correlated to those reaction conditions are still mysterious due to the susceptible internal interactions happened in soot formation process.

To further understand the physicochemical mechanism of soot formation, plenty of studies have been carried out to inquire into the influential factors of soot properties. Trubetskaya et al. [19] studied the effect of different feedstock and pyrolysis temperatures on soot properties which are mainly nanostructure, and found out that high temperature and high content of potassium strongly influenced the soot reactivity in CO₂ gasification. Vander Wal and Tomasek [20] addressed the differences in soot nanostructure based upon formation and growth condition, stating a change between amorphous soot structure and a highly curved nanostructure when temperature, flow rate and fuel species changed. Böhm et al. [21] modeled the pyrolysis of acetylene and benzene at high temperatures and pressures and found a similar activation energy for high molecular PAH and soot formation, further concluding that soot mass growth rates were strongly related to PAH formation. However, with many studies investigating the soot formation mechanisms of biomass, coal and liquid or gaseous hydrocarbons, studies concentrating on soot products obtained from plastics are rare, among which studies on PU plastic are extremely lacking. What's more, though few present studies [22, 23] have worked on soot formation of PU, the most common method adopted was combustion, and the soot was mainly generated in flame. Overall, the soot formation mechanism during PU pyrolysis under a relatively high temperature (> 1200 °C) is poorly understood.

To our knowledge, no previous efforts have been made to determine how the pyrolysis conditions including temperature and residence time influence PU pyrolysis soot product yield and soot properties. In this study, PU pyrolysis cases with different pyrolysis temperatures and residence times were carried out. The objective of this study is to determine the effect of varied temperatures and residence times on product yield and soot properties including micro-morphology, physiochemical structure, surface functionality and oxidation reactivity. Based on the obtained knowledge, a specific soot formation pathway indicating soot formation mechanism during PU pyrolysis is suggested.

2. Materials and methods

2.1. Materials

Polyurethane used in this study was wasted PU plastic previously used as an insulation material inside refrigerators, collected from Croatia. The ultimate/proximate analyses and the ash composition analysis are shown in Table 1 and Table 2, respectively. PU samples contained high contents of oxygen (24.0 wt.%), nitrogen (6.4 wt.%) and volatile (83.2 wt.%), The Fe, Ti, Si, and Al contents were abundant in ash, and the sum of Na and K contents is 3.7 wt.%. Considering the samples were obtained from wasted foams, it is reasonable that PU samples were partly contaminated. The raw sample was first milled and sieved into the diameter of 50-100 µm, then dried at 105 °C for 24h in an oven before use.

Table 1. Ultimate and proximate analyses of polyurethane									
Ultimate ana	lysis (wt.%)		Proximate analysis (wt.%)						
C_{ad}	H_{ad}	O_{ad}	N_{ad}	S _{ad}	V_{ad}	FC_{ad}	A_{ad}		
62.7	6.3	24.0	6.4	0.6	83.2	10.6	6.2		

(V_{ad}: volatile matter as air dried basis; FC_{ad}: fixed carbon as air dried basis; A_{ad}: ash as air dried basis).

Table 2. Ash composition analysis														
Sample	Fe ₂ O ₃	TiO ₂	SiO ₂	CaO	ZnO	Al_2O_3	Na ₂ O	MgO	SO ₃	BaO	K_2O	P_2O_5	CuO	Cl
Polyurethane	31.5	23.4	10.4	7.1	6.0	3.4	2.7	2.6	1.3	1.1	1.0	0.9	0.4	0.3

2.2. Experimental apparatus and procedure

2.2.1. Fixed-bed reactor

In this study, pyrolysis experiments were conducted in two fixed-bed reactor systems where different sets of reactors were adopted to realize different residence times of volatiles in the reactor tube. A longer quartz tube with length of 1500 mm was set in a large horizontal-chamber furnace to realize a long residence time of 2 s, a small one with length of 800 mm in a small furnace to realize a short residence time of 0.2 s. 2 s is the normal residence time of flue gas in the furnace, while 0.2 s is the lower limit we can control through the reactor and sampling probe design. The internal diameter of both quartz tubes was 30 mm. As shown in Fig. 1, from left to right are the nitrogen control unit, the temperature control unit, the quartz reactor unit, the soot collecting unit, the tar condensation unit, the gas filter and dryer unit, and the metering and analyzing unit.

The reactors were heated to target temperatures (1000, 1100, 1200, and 1300 °C) with the N₂ flow of 4 L min⁻¹ to create an inert atmosphere, and samples with a mass of 1 ± 0.005 g contained in a corundum boat were placed in the cool region of the reactor tube in N₂ atmosphere before experiments began. Below 1000 °C, there will be excessive tar in the reactor, adhering on the inner wall of reactor and sampling tube, which will significantly affect the accurate sampling of soot. 1300 °C is the upper limit at which the furnace can long-time run. After 30 min when a constant temperature and purely inert atmosphere (N₂ content > 99.9 wt.%) were obtained, the corundum was pushed into the constant-temperature reaction zone and rapidly pyrolyzed. The pyrolysis process of each sample lasted for 10 min which is an appropriate time that has proven to ensure the completion of total gas release. After that the quartz boat was pulled back to the cool region, cooled to room temperature in the N₂ atmosphere, and the solid residue was collected.

The soot collecting unit was heated to ~250 °C which was 50 °C higher than that in the work of Trubetskaya et al. [24] to avoid the condensation of tar products, and the soot collected was preserved for further characterization. The outlet of reactor was covered with PU materials for heat insulation to avoid overcooling of tar vapors, and the tar condensation unit consists of three tandem vessels containing dichloromethane cooled in the iced water to collect the condensable bio-oil. The volume of non-condensable gas was calculated when passing through a gas flow meter. A suitable amount of gas was separated by a three-way valve, collected by a gas bag and preserved. Each experiment was repeated two or three times to ensure the repeatability.



Fig. 1 Fixed-bed reactor system

2.2.2. Product yields measurement

The collected soot and char can be directly weighed by an electronic balance. The exhausted pyrolysis gases after condensation treatment, collected in gas bags, were then analyzed by a gas chromatograph (GC, GC-2014, Shimadzu, Japan) to quantify the concentrations of CO₂, CO, H₂, CH₄, and C₂H_m (C₂H₂, C₂H₄ and C₂H₆). Knowing the N₂ gas flow,

experimental time and gas concentration in the gas sample bags, the mass of other gases could be calculated, and the total gas yield could be further calculated. The quantity of the liquid fraction, including bio-oil and water, was calculated from the mass balance. The tar compositions were identified by a gas chromatograph-mass spectrometer (GC-MS, QP2010 Ultra, Shimadzu, Japan).

2.2.3. Soot characterization

Soot samples used for characterization analyses were first treated by ultrasonic extraction in dichloromethane solvent for 5 min, and then centrifugalized three times. Soot morphologies were observed by high-resolution transmission electron microscope (HR-TEM, JEM-2100, JOEL, Japan), and the crystal property was investigated by the X-ray diffraction (XRD, X'pert MPD Pro, PAN-alytical, Netherlands).

As a toxic pollutant, the oxidation reactivity of soot is important for its consumption and controlling. Therefore, the soot oxidation reactivity was investigated by thermogravimetric analyzer (TGA, STA-409PC, NETZSCH, German). For each test, approximately 5 mg of soot sample was placed in a corundum crucible and heated at a heating rate of 20 K min⁻¹ from room temperature to 1273 K in air atmosphere environment (20 vol.% O₂/80 vol.% N₂) with a total flow rate of 100 ml min⁻¹. All tests were performed under the same conditions to guarantee the comparability. The mass loss (TG) curves and differential thermogravimetric (DTG) curves were online-recorded.

3. Results and discussion

3.1. Soot, gas, char and tar yields

The yield of soot/gas/tar/char products as pyrolysis temperature varied in 1000-1300 °C with different residence times were illustrated in Figs. 2(a) and 2(b), respectively. With a residence time of ~2 s, as shown in Fig. 2(a), a soot yield of 11.1 wt.% was obtained under 1000 °C. An obvious positive correlation can be observed between increasing temperature from 1000 °C to 1300 °C and soot yield which reached to 24.5 wt.% under highest temperature. This result coincides well with some previous studies [25, 26] that have concluded the increasing temperature strengthened the thermal cracking and decomposition reactions of heavy hydrocarbons in tar into lighter radicals, and these radicals (mainly C₂-C₆ compounds) were then polymerized and formed PAH compounds, and functioned in soot formation process. Note that some simultaneous interactions happening along with soot nucleation and surface growth which were the reason to soot quantity increase, that is, thermal cracking of soot chemical structures and partial oxidation by oxygen-containing radicals (-OH, -C=O-, etc.), might be contributions to potential soot quantity decrease when temperature continuously rises [27]. Considering the high content of oxygen in PU samples which is 24.01 wt.% as shown in Table 1 and the relatively high contents of CO/CO₂ in pyrolysis gases, these negative reactions for soot formation might not be neglected.

Flecher et al. [17] have stated a favored polymerization reaction over cracking and oxidation reactions when soot formed lower than 2000 K, promising the increase of soot in quantity.



Fig. 2 The effect of pyrolysis temperature on product yields: (a) residence time-2s; (b) residence time-0.2s.

In Fig. 2(a), the tar yield is observed to decrease from 33.3 wt.% at 1000 °C to 19.0 wt.% at 1300 °C, which corresponds well with the explanation above, that the reduction of tar content is mainly ascribed to the instability of heavy hydrocarbons under relatively high temperatures. The majority of primary hydrocarbon compounds in pyrolysis volatiles are aliphatic and aromatic hydrocarbons, according to Chen et al. [28], aliphatic compounds are unstable under high temperature and are easily broken into small molecules, while aromatic ring structures are relatively stable and tends to polymerize into PAHs. The broken molecular radicals then incline to develop into small gaseous components that lead to an increase in gas yield, part of which also participates in soot formation [29]. The yield of pyrolysis gas increases from 36.3 wt.% at 1000 °C to 40.6 wt.% at 1300 °C. A slight change from 19.5 wt.% at 1000 °C to 15.9 wt.% at 1300 °C is observed in char yield when temperature increases. This is mainly due to the limited volatile content in PU samples that can be released during pyrolysis. In summary, increasing temperature enhances thermal cracking of raw PU samples and slightly increases the release of volatiles, leading to a slight decrease in char yield. Higher temperature enhances the reforming and decomposition of volatile species and thus brings about decreased tar yield, and increases light gases and hydrocarbons.

Fig. 2(b) shows the distributions of pyrolysis products obtained under increasing temperature with a shorter residence time of 0.2 s. By comparison, it can be observed that the changing trends of pyrolysis products as the temperature increasing between pyrolysis cases with long and short residence times are similar, however, the product yield distributions are different. As shown in Fig. 2(b), soot only forms when temperature increases to 1200 °C which is a much higher initial temperature of soot occurrence compared to that in Fig. 2(a) with a longer residence time of 2 s. At 0.2 s, the soot and gas yields are lower than those in the pyrolysis with a longer residence time, while the tar yield is

significantly higher. This can be ascribed to the limited residence time in the high temperature region of the released volatiles from PU samples, and thus the thermal cracking and decomposition reactions of volatile compounds were deficient. After undergoing secondary reactions of volatiles at high temperatures, small PAH compounds grow into larger ones of molecular weights 500-1000. Condensation begins when the PAHs grow to the size of four rings and larger, collision giving birth to the formation of small clusters. The simultaneous condensation and the PAH growth finally lead to the formation of soot particles, or described as 'soot precursor'. Consequential lack of intermediate, accompanied with insufficient reacting time for volatile secondary reactions directly leads to significantly declines in soot yield which highly relies on the grow from PAHs to soot precursor, and in gas yield which is mainly dominated by the breaking of large hydrocarbons into small molecular radicals and further development into small molecular gas species [28]. The minor difference between char products at different volatile residence time. It can be explained by the sorption of volatile organic compounds due to the micro-porous structure and abundant surface functional groups of char itself [30, 31]. A longer volatile residence time means more contact between char and volatiles, more sorption of organic compounds and thus higher weight.

3.2. Soot characterization

3.2.1. Soot micro-morphologies

The micro-morphologies of soot particles collected under different temperatures and residence times were obtained by HR-TEM, as shown in Table 3. At a residence time of 2 s, the soot collected from pyrolysis at 1000 °C consists of primary particles whose diameters ranged from 200-500 nm, indicating the morphologies of an aggregated cluster in irregular shapes with diameters of 1-2 µm. Surrounding the particles of spherical nuclei agglomerating together are structures with higher transparency in TEM images that show smooth edges and curved surfaces. Similar results were obtained from both TEM and AFM by Abid et al. [18] who used 'halo' to define the coating structures, indicating that the particles were not solid but liquid-like tar-balls, and under the impact of TEM substrate they would spread over the surface. This morphology implies the unfinished carbonization process during which the liquid-like precursor particles solidified, involving the conversion of PAH contents with high hydrogen mole fraction to highly carbonized ones. As comparison, the soot particles from pyrolysis at 1100 °C and 1200 °C are much better-defined with smaller sizes (50-200 nm) but still contain a certain number of larger irregular particles (~200 nm). When temperature reaches 1300 °C, a large portion of irregular large particles disappear, while larger amounts of regular, distinct spherical-boundary fine particles (30-150 nm) dominate. When comparing the enlarged views of soot particles obtained under these four temperatures, the stacking of the graphite layers results in disordered internal structures as observed from images of soot particles at

1000 °C and 1100 °C, while regular soot structures with parallel, ordered graphite layers around a core, i.e., onion-like structures, can be distinguished at 1200 °C and 1300 °C. Hence, it can be concluded that a higher temperature contributes to an enhanced soot carbonization degree.

Morphologies of soot particles also significantly changed when the volatile residence time changes from 2 s to 0.2 s, as shown in Table 3. At the same pyrolysis temperatures, soot particles obtained from the case of 0.2 s show much more disordered and liquid-like surfaces which indicated inadequate development and carbonization, compared to those from pyrolysis case of 2 s. This means the shorter residence time impaired the positive effect of high temperature on soot formation and development, resulting in that the soot particles at high temperatures and the short volatile residence time showed similar morphologies with those at lower temperatures and the long volatile residence time. This phenomenon might be ascribed to two reasons: (1) the shorter residence time weakens the decomposition and cracking process of volatile compounds, thereby produces less active radicals attached on soot surfaces, and diminishes the contact between soot precursor and the volatile species, thus generating agglomerates consisting of nascent soot particles instead of well-developed soot particles [32]; (2) the shorter residence time of soot in high temperature environment directly restricts the carbonization process of soot particles [33].

1	Table 3 M	licro-morphologies of nano-scale	soot particles produced at varied	l temperatures and residence time	28
Residence time	Pyrolysis temperature	1000 °C	1100 °C	1200 °C	1300 °C
~2s	Scale=200 nm	200 µm	200 µm	200 µm	<u>200 µm</u>
	Scale=5 nm	5 m	Sμm	S m	5μm
~0.2s	Scale=200 nm	None	None	<u>200 µп</u>	<u>200 µп</u>
	Scale=5 nm	None	None	5 μm	Sμm

2 3.2.2. XRD patterns

3 XRD patterns of soot particles obtained in the temperature range of 1000-1300 °C are characterized and shown in Fig. 3. 4 The broad reflections at 24.2° and 43.3° indicate the development of a crystalline phase which is assigned to the parallel 5 graphite layers, representing the highly carbonized onion-like soot structure observed in TEM morphologies. Similar 6 results have been reported by Trubetskaya et al. [19] who claimed that the reflection at 25° spaced at a well-defined 7 inter-planar distance represented the parallel graphene layers while the reflection at 43.6° representing two-dimensional 8 reflections indicating the ordering of carbon atoms inside the graphite layers. It can be seen from Fig. 3 that the featured 9 peak height significantly increases when temperature increases from 1000 °C to 1100 °C, and from 1100 °C to 1200 °C 10 as well, however, this increase is very modest when temperature increases from 1200 °C to 1300 °C. This result agrees 11 well with the morphologies by TEM, indicating that 1100 °C is a critical temperature when the graphite layer structures 12 begin to occur and develop.



13 14

Fig. 3 XRD analysis of soot particles from 1000-1300 °C.

Besides the obvious reflections at 24.2° and 43.3° , two small sharp peaks are also observed at 31.7° and 45.5° , 15 16 respectively, only at 1200 °C and 1300 °C. The XRD analysis indicates that these two peaks represent the existence of 17 NaCl in soot particles. The selectively occurrence of NaCl in relatively high temperatures indicates that the Na in plastic 18 waste at high temperatures can evaporate and combine with Cl to form NaCl molecular, and then condensed into NaCl 19 crystals with the temperature decreasing. Li et al [34] has reported the increasing release of gaseous potassium with 20 increasing temperature, indicating a similar release mechanism of metal species at high temperatures. Di Stasio et al. [35] 21 and Trubetskaya et al. [19] have reported the inhibition of coagulation and agglomeration of soot particles due to charge 22 exchange with the existence of alkali and alkaline earth metallic species (AAEMs). This statement highly agreed with the 23 result of TEM where soot particles from 1200 °C and 1300 °C showed evidently smaller particle sizes and less 24 agglomeration property, as shown in Table 3.

25 3.2.3. Soot reactivity

26 The oxidation reactivity of soot is important for the control of trace soot emission during incineration process, as well as 27 the performances of soot products used in different industries. In this part, the oxidation reactivity of soot in air 28 atmosphere environment of 20 vol.% O₂/80 vol.% N₂ was tested by a non-isothermal TGA. The measured TG-DTG 29 curves and Arrhenius kinetic plotting are shown in Fig. 4, and the characteristic parameters are summarized in Table 4, 30 where T_s (°C) is the start temperature of soot oxidation, T_{peak} (°C) is the peak temperature of DTG curves, T_f (°C) is the 31 finish temperature of soot oxidation, w_{max} is the maximum mass loss rate or the peak height of DTG curves, E (kJ mol⁻¹) 32 is the apparent activation energy and $A(s^{-1})$ is the pre-exponential factor of soot oxidation. The definition methods of 33 these characteristic parameters can be found in our previous work [36].







Fig. 4 (a) TG-DTG curves and (b) Arrhenius plotting of soot oxidation.

As shown in Fig. 4(a), when the pyrolysis temperature increases from 1000 °C to 1100 °C, TG-DTG curves significantly 37 38 shifted right with T_i, T_{peak}, and T_f increasing by 49 °C, 58 °C, and 38 °C, respectively. However, while the pyrolysis 39 temperature further increases from 1100 °C to 1200 °C, T_i decreases by 11 °C, T_{peak} showing no change and T_f even 40 decreasing by 22 °C, which results in a more drastic mass loss ratio. When the pyrolysis temperature increased from 41 1200 °C to 1300 °C, TG-DTG curves slightly shift right, and these three characteristic temperatures increased by 3-7 °C. 42 As for the mass loss rate or kinetic parameters, shown in Table 4, with the increase of pyrolysis temperature in the range 43 of 1000-1300 °C, the increases of w_{max} , E, and A can be observed. When the pyrolysis temperature increases to the range 44 of 1200-1300 °C, the apparent activation energy is relatively stable at the range of 159-181 kJ mol⁻¹.

The measured results of soot oxidation reactivity at different pyrolysis temperatures can be explained by the micro-morphologies of soot particles introduced in Table 3. (1) At 1000 °C, particles exist as liquid-like phase but with much larger diameters than those produced at higher temperatures, which results in much lower characteristic temperatures and higher oxidation reactivity. The composition of those not well carbonized soot particles is complex with a relatively low contents of carbon [20], some components in which require a high temperature to burn out, contributing 50 to a wide distribution of DTG peak, in respect to a heterogeneous soot mixture with varied compositions and particle size 51 distribution [37]. (2) Pyrolysis temperature increasing to 1100 °C gives birth to a large amount of well-developed, 52 spherical solid-phase finer soot particles with developed, more aromatic hydrocarbon structures which are much more 53 difficult than liquid-like particles to be oxidized [38]. On the other hand, there are still a non-negligible number of 54 liquid-like particles. This demonstrates the reason of DTG curve of soot sample of 1100 °C maintaining a wide 55 distribution and a modest mass loss rate. (3) When the pyrolysis temperature increases to 1200 °C and 1300 °C, the soot 56 particles dominantly exist in the form of nanoscale soot particles with ordered and relatively fine sizes and uniform 57 chemical compositions, while those disordered large liquid-like particles with complicated compositions almost 58 disappeared, leading to a decreased finish temperature.

Additionally, another important factor affecting the performances of soot oxidation is the existence of NaCl in soot products. XRD patterns in Fig. 3 have proved the existence of NaCl in soot particles from PU pyrolysis at higher than 1100 °C, which might play the role of catalyst during soot oxidation process. According to Neeft et al. [39], the intensity of contact between soot and alkali metals is a major predictor of soot oxidation rate. Thus, the resulted salience of soot samples from 1200 °C and 1300 °C in significantly higher oxidation reactivity, indicated by the left-shifting TG curves and promoted DTG peaks, explained by possible catalytic effect, was reasonable. Similar result has been observed in the work of Wang et al. [36].

When pyrolysis was conducted at a shorter residence time of 0.2 s, the soot products obtained at 1200 °C and 1300 °C showed relatively higher oxidation reactivity compared with those with a residence time of 2 s. As listed in Table 4, with the same pyrolysis temperature, these characteristic parameters of soot oxidation at 0.2 s are all lower than those at 2 s. This result aligns well with the morphology results in Table 3, that the soot particles produced at the shorter residence time are more liquid-like, indicating a better oxidation reactivity.

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Table 4 The summary of characteristic parameters in all studied cases.

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	Residence time	Pyrolysis temperature	$T_{ m i}$	$T_{\rm peak}$	$T_{ m f}$	W _{max}	Ε	Α	R^2	
	S	°C	°C	°C	°C	%/min	kJ mol ⁻¹	1/s	1	
_		1000	518	559	614	9.9	69.9	521.6	0.923	
2	1100	567	617	652	11.6	97.1	38812	0.993		
	1200	578	617	630	19.5	159.3	2.5E10	0.991		
	1300	585	620	634	20.2	181.1	1.8E12	0.992		
0.2	1200	521	580	613	9.6	82.6	5595	0.973		
	1300	532	602	634	14.8	80.2	1586	0.997		

72 **3.3.** Gas composition

73 The compositions of pyrolysis gases and their distribution changes with increasing temperature at two residence times are 74 shown in Figs. 5(a) and 5(b), respectively. From Fig. 5(a), a dominant amount of H₂ content which is 51.7 vol.% at 75 1000 °C and 69.8 vol.% at 1300 °C can be observed. This abundance of H₂ in pyrolysis gases was mainly due to the 76 facilitated cyclization and aggregation reactions when temperature increases during soot formation and growth. The 77 small molecules not only attach to the surface of soot particles but also join to each other and formed small aromatic 78 compounds at the cost of release of H atoms, and further formation of H_2 , known as hydrogen abstraction [29]. The slight 79 decrease of CH₄, C₂H₂ and C₂H₄ contents match well with this explanation. The CO content increases from 15.8 vol.% at 80 1000 °C to 25.0 vol.% at 1300 °C, while on the contrary the content of CO₂ decreases from 12.9 vol.% at 1000 °C to 2.1 81 vol.% at 1300 °C. This result can be mainly explained by the facilitated oxidation of soot when temperature increases. 82 Along with other oxidative radicals, CO_2 in gas phase might play an important role as oxidant at high temperature, 83 partially oxidizing soot particles, leading to a decrease in CO₂ content but an increase in CO content.

Fig. 5(b) shows the gas compositions at a shorter volatile residence time of 0.2s. Similarity in the developing trend of same gaseous species to that in Fig. 5(a) is observed, while the content of each component is not completely consistent. When pyrolysis happens at the same temperature, a lower H_2 content as well as a higher CO content at a shorter residence time can observed, while other components show only marginal increase. This was mainly due to the diminished secondary reactions in volatile phase that inhibit the hydrogen abstraction reaction and further H_2 release, resulting in the consequent decrease of H_2 content and increase of other gas species' contents.



90

Fig. 5 The effect of pyrolysis temperature on gas product compositions: (a) 2 s; (b) 0.2 s.

91 **3.4. PAHs in tar products**

92 The detectable compounds in tar from PU pyrolysis at temperature of 1000-1300 °C are listed in Table 5, and 93 summarized in Table 6 in terms of 'aromatic ring number' to determine the development of PAH compounds. The

94 generally expected liquid product should be a very complex mixture of organic compounds containing mainly aromatic 95 compounds as well as noticeable aliphatic compounds and heterocyclic nitrogen-containing and oxygen-containing 96 species [40]. However, at the relatively high pyrolysis temperature in this study, only trace amount of those 97 nitrogen-containing and oxygen-containing compounds are detected. Herrera et al. [41] reported further decompose of 98 PU samples to smaller compounds and the release of nitrogen content in the form of nitrogen-containing products like 99 HCN, acetonitrile, etc. Zhang el al. [2] adopted a model compound method to investigate the thermal degradation of PU 100 materials and found out the thermal breaking of C-O and C-N bonds during pyrolysis. Therefore, the absence of 101 heterocyclic compounds in tar can be mainly attributed to the breaking of C-O and C-N bonds at such high temperatures 102 and the release of small molecular gaseous compounds (CO, CO_2 , NO_3 , HCN, etc.) [42]. The disappearance of aliphatic 103 compounds, according to our previous research [13], is mainly a result of high temperature and long volatile residence 104 time.

105 A significant decrease in the amount of tar species can be observed from Table 5 when the pyrolysis temperature 106 increases. This change implies that the temperature increasing enhances the depolymerization and aromatization 107 reactions of volatile compounds, resulting in the transformation from higher reactivity compounds to highly 108 thermal-stable PAHs, such as perylene, benzo[e]pyrene, naphthacene, etc. This trend is clearly exhibited in Table 6 109 where the distribution of tar composition ring numbers is highly related to the pyrolysis temperature [13]. In the studied 110 temperature range, at 1000 °C and 1100 °C, the species of ring number ≥ 5 are rarely observed in tar products, and the tar 111 composition is dominated by the species of ring number ≤ 4 . However, when the pyrolysis temperature increases to 1200 °C and 1300 °C, the overall content of species of ring number \geq 4 becomes over 50 wt.%. 112

113

Table 5 Tar compositions at varied pyrolysis temperatures (1000-1300 °C)

No.	Compound	Formula	Structural formula	1000 °C	1100 °C	1200 °C	1300 °C
1	Benzene,-1-ethenyl-4- methyl-	C ₉ H ₁₀		-	0.97	-	-
2	Naphthalene	$C_{10}H_8$		15.13	-	-	-
3	Biphenyl	$C_{12}H_{10}$		1.27	-	-	-
4	Biphenylene	$C_{12}H_8$		12.57	2.27	-	-
5	Fluorene	$C_{13}H_{10}$		1.42	-	-	-
6	Phenanthrene	$C_{14}H_{10}$		24.3	14.81		5.34
7	Anthracene	$C_{14}H_{10}$		-	2.8	10.23	0.94
8	1,4-Ethenoanthracene, -1,4-dihydro-	C ₁₆ H ₁₂		-	-	-	1.92
9	4H-Cyclopenta[def]p henanthrene	C ₁₅ H ₁₀		1.36	1.95	-	-
10	Naphthalene,-2-pheny l-	C ₁₆ H ₁₂		0.93	0.48	-	-
11	Fluoranthene	$C_{16}H_{10}$		22.60	54.49	11.04	-
12	Perylene	$C_{20}H_{12}$		-	-	42.23	-
13	Benzo[e]pyrene	C ₂₀ H ₁₂		-	0.69	-	32.45
14	Pyrene	C ₁₆ H ₁₀		-	-	-	0.78
15	Benz[e]acephenanthry lene	$C_{20}H_{12}$		-	-	-	7.43

16	Benzo[c]phenanthren e	C ₁₈ H ₁₂		-	0.38	-	-
17	Benzo[ghi]fluoranthe ne	C ₁₈ H ₁₀	X	5.16	20.09		-
18	Benz[a]anthracene	$C_{18}H_{12}$		-	0.57	10.54	-
19	Naphthacene	$C_{18}H_{12}$		1.7	-	-	1.12
20	Triphenylene	C ₁₈ H ₁₂		2.29	-	3.53	10.24

1	1	5
1	1	6

Table 6. Tar composition profiles by 'ring number' at 1000-1300 °C								
Aromatic ring number	1000 °C	1100 °C	1200 °C	1300 °C				
1	0.00	0.97	0.00	0.00				
2	30.39	0.00	0.00	0.00				
3	49.19	20.36	21.27	8.2				
4	3.99	57.39	14.07	19.57				
≥5	0.00	0.00	42.23	32.45				

117 **3.5.** Pathway of soot formation during PU pyrolysis at high temperatures

Based on the above characterization results of soot, gas and tar products, a reaction pathway of soot formation during PU pyrolysis at high temperatures is proposed in Fig. 6. When undergoing thermal cracking at high temperatures, the molecular structures of polyurethane polymer start to break down and 4,4'-diphenylmethane diisocyanate, considered as the dominant intermediate during prior cracking process. Subsequently the scission of carbon-nitrogen and carbon-oxygen bonds occurs [2], 4,4'-diphenylmethane diisocyanate degrading into 4,4-diaminodiphenyl methane with the release of CO and CO₂ gases.

Then after undergoing secondary reactions in the form of volatiles in the high temperature region of the reactor, small PAH compounds with 1-5 aromatic rings grow into larger PAHs of molecular weights 500-1000 via the interactions known as HACA mechanism [15] and "ring-ring condensation" interaction (under sufficient aromatic species concentration only) [16]. It is worth noting that the two pathways are not isolated but co-constructing to build up the PAHs growth mechanism. Condensation begins when the PAHs grow to the size of four rings and larger, collision giving birth to the formation of small clusters. The simultaneous condensation and the PAH growth finally lead to the formation of soot particles, or described as 'soot precursor'. This process is known as particle inception [17, 18, 43]. The development of soot after the particle inception is mainly dominated by: (1) the surface growth in which gas-phase species are attached to the surface of a particle, leading to an increase of soot amount without changing particle numbers, and (2) coagulation where particles collide and coalesce, leading to the decrease of number density. Remarkably, only 10 wt.% of the soot mass is produced during the inception period whereas as much as 90 wt.% of the total comes from surface growth [43]. At final stages, the discernable primary particles are chemically fused together, known as agglomerate. The morphology of soot particles, whose diameters are about 20-100 nm, in terms of chains, clusters, dendrites, rings, spheroids, flakes and other types, is observed.





Fig. 6 The formation pathway of soot during PU pyrolysis.

140 4. Conclusions

(1) The initialization and growth of soot particles during PU pyrolysis requires a certain high temperature and long
volatile residence time. With a volatile residence time of 2 s, the soot yield is 11.0 wt.% at 1000 °C and increases to
24.5 wt.% when the pyrolysis temperature increases to 1300 °C. In contrast, with a short volatile residence time of

0.2 s, the soot cannot be observed until 1200 °C. The increase of pyrolysis temperature increases the soot and gas
yields while decreases the tar and char yields. The decrease of volatile residence time decreases the soot, gas and
char yields while increases the tar yield. The soot formation pathway during PU pyrolysis at higher temperatures can
be reflected by the gas and tar composition measurement.

(2) The soot morphology and reactivity are significantly affected by the pyrolysis temperature and volatile residence time. More carbonized and ordered structures with distinguishable parallel graphitic layers are observed in the soot particles produced from higher temperature or longer residence time. The temperature about 1100 °C is a critical temperature for soot formation, beyond which the parallel layered structures begin to form. When the volatile residence time decreases from 2 s to 0.2 s, the oxidation reactivity of soot decreases. The NaCl coexisting with soot is observed by XRD when the pyrolysis temperature increases from 1100 °C to 1200 °C, which catalytically promotes the soot oxidation.

155 Acknowledgements

156 The authors gratefully acknowledge the financial support of the National Natural Science Foundation of China (Nos.

157 51676157 and 5161101654), and the National Key Research and Development Program of China (No. 2017YFB0603902).

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